## CLAIMS

What is claimed is:

1. A method, a sensor array that employs a parameter to induce a time-varying phase angle $\varphi$ on an optical signal that comprises a phase generated carrier with a demodulation phase offset $\beta$, the method comprising the step of:

calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$.

2. The method of claim 1, further comprising the step of:

sampling an output signal from the sensor array to obtain a plurality of samples $S_n$, wherein $n = 0$ to $x$;

wherein the step of calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ comprises the step of:

calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of one or more of the plurality of samples $S_n$.

3. The method of claim 1, wherein the step of calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of the one or more of the plurality of samples $S_n$ comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples $S_n$, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$; and

calculating the phase angle $\varphi$ through employment of the one or more quadrature terms and the one or more in-phase terms.

4. The method of claim 2, wherein the output signal comprises a period $T_{pulse}$, wherein the step of sampling the output signal from the sensor array to obtain the plurality of samples $S_n$, wherein $n = 0$ to $x$ comprises the step of:

sampling the output signal from the sensor array to obtain a plurality of samples $S_n$ within a period $T_s$, wherein $n = 0$ to $x$, wherein $T_s$ is less than or equal to $1.125 \times T_{pulse}$.

5. The method of claim 4, wherein $T_s$ is less than or equal to $T_{pulse}$.

6. The method of claim 4, wherein the step of calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of the one or more of the plurality of samples $S_n$ comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples $S_n$, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$;

calculating the phase angle $\varphi$ through employment of the one or more quadrature terms and the one or more in-phase terms.

7. The method of claim 6, wherein the step of calculating the one or more quadrature terms and the one or more in-phase terms through employment of the one or more of the plurality of samples $S_n$, wherein the one or more of the one or more quadrature terms and the one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$ comprises the steps of:

calculating a set of quadrature terms $Q_j$ and a set of in-phase terms $I_k$ through employment of one or more of the plurality of samples $S_n$, wherein $j = 0$ to $y$, wherein $k = 0$ to $z$;

calculating a quadrature term $Q_{ab}$ from a largest term of absolute values of the set of quadrature terms $Q_j$;

calculating a constant $C_1$ and a constant $C_2$;

calculating a quadrature term $Q_s = C_1 \times \sqrt{\sum_{j=0}^{j=y} Q_j^2}$, wherein $Q_s$ is substantially independent from the demodulation phase offset $\beta$; and

calculating an in-phase term $I_s = C_2 \times \sqrt{\sum_{k=0}^{k=z} I_k^2}$, wherein $I_s$ is substantially independent from the demodulation phase offset $\beta$.

8. The method of claim 7, wherein the step of calculating the constant $C_1$ and the constant $C_2$ comprises the step of:

calculating the constant $C_1$ and the constant $C_2$ such that an amplitude of the quadrature term $Q_s$, an amplitude of the quadrature term $Q_{ab}$, and an amplitude of the in-phase term $I_s$ comprise a substantially same amplitude for a modulation depth M of an operating range for the phase generated carrier.

9. The method of claim 7, wherein $x = 7$, $y = 3$, $z = 1$, wherein the step of calculating the set of quadrature terms $Q_j$ and the set of in-phase terms $I_k$ through employment of the one or more of the plurality of samples $S_n$, wherein $j = 0$ to $y$, wherein $k = 0$ to $z$ comprises the steps of:

calculating $Q_0 = S_0 - S_4$;

calculating $Q_1 = S_1 - S_5$;

calculating $Q_2 = S_2 - S_6$;

calculating $Q_3 = S_3 - S_7$;

calculating $I_0 = ( S_0 + S_4 ) - ( S_2 + S_6 )$; and

calculating $I_1 = ( S_1 + S_5 ) - ( S_3 + S_7 )$.

10. The method of claim 7, wherein $x = 15$, $y = 7$, $z = 3$, wherein the step of calculating the set of quadrature terms $Q_j$ and the set of in-phase terms $I_k$ through employment of the one or more of the plurality of samples $S_n$, wherein $j = 0$ to y, wherein $k = 0$ to z comprises the steps of:

calculating $Q_0 = S_0 - S_8$;

calculating $Q_1 = S_1 - S_9$;

calculating $Q_2 = S_2 - S_{10}$;

calculating $Q_3 = S_3 - S_{11}$;

calculating $Q_4 = S_4 - S_{12}$;

calculating $Q_5 = S_5 - S_{13}$;

calculating $Q_6 = S_6 - S_{14}$;

calculating $Q_7 = S_7 - S_{15}$;

calculating $I_0 = ( S_0 + S_8 ) - ( S_4 + S_{12} )$;

calculating $I_1 = ( S_1 + S_9 ) - ( S_5 + S_{13} )$;

calculating $I_0 = ( S_2 + S_{10} ) - ( S_6 + S_{14} )$; and

calculating $I_1 = ( S_3 + S_{11} ) - ( S_7 + S_{15} )$.

11. The method of claim 7, wherein the step of calculating the phase angle $\varphi$ through employment of the one or more quadrature terms and the one or more in-phase terms comprises the steps of:

calculating a correction term $\Delta Q$;

calculating a quadrature term $Q_m$ from the quadrature term $Q_s$ and the correction term $\Delta Q$;

calculating a quadrature term Q from a magnitude of the quadrature term $Q_m$ and one or more quadrature terms of the set of quadrature terms $Q_j$;

calculating an in-phase term I from a magnitude of the in-phase term $I_s$ and one or more in-phase terms of the set of in-phase terms $I_k$; and

calculating the phase angle $\varphi$ from an arctangent of a quantity $Q / I$.

12. The method of claim 11, wherein the step of calculating the correction term $\Delta Q$ comprises the step of:

calculating the correction term $\Delta Q = Q_s - Q_{ab}$.

13. The method of claim 11, wherein the step of calculating the quadrature term $Q_m$ from the quadrature terms $Q_s$ and $\Delta Q$ comprises the step of:

calculating a constant $C_3$; and

calculating $Q_m = Q_s + (C_3 \times \Delta Q)$.

14. An apparatus, a sensor array that employs a parameter to induce a time-varying phase angle φ on an optical signal that comprises a phase generated carrier with a demodulation phase offset β, the apparatus comprising:

a processor component that calculates the phase angle φ independent from the demodulation phase offset β.

15. The apparatus of claim 14, wherein the processor component obtains a plurality of samples $S_n$ of an output signal from the sensor array, wherein $n = 0$ to $x$;

wherein the processor component employs one or more of the plurality of samples $S_n$ to calculate the phase angle φ independent from the demodulation phase offset β.

16. The apparatus of claim 15, wherein the processor component employs one or more of the plurality of samples $S_n$ of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset β of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle φ.

17. The apparatus of claim 15, wherein the output signal comprises a period $T_{pulse}$, wherein the processor component obtains the plurality of samples $S_n$ within a period $T_s$, wherein $T_s$ is less than or equal to $1.125 \times T_{pulse}$.

18. The apparatus of claim 17, wherein $T_s$ is less than or equal to $T_{pulse}$.

19. The apparatus of claim 17, wherein the processor component employs one or more of the plurality of samples $S_n$ of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$ of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle $\varphi$.

20. The apparatus of claim 19, wherein the one or more of the one or more quadrature terms comprise a quadrature term $Q_{ab}$ and a quadrature term $Q_s$, wherein the one or more of the one or more in-phase terms comprise an in-phase term $I_s$;

wherein the processor component employs one or more of the plurality of samples $S_n$, the quadrature term $Q_{ab}$, the quadrature term $Q_s$, and the in-phase term $I_s$ to calculate the phase angle $\varphi$.

21. The apparatus of claim 20, wherein the processor component employs the plurality of samples $S_n$ to calculate a set of quadrature terms $Q_j$ and a set of in-phase terms $I_k$, wherein j = 0 to y, wherein k = 0 to z;

wherein the processor component employs the set of quadrature terms $Q_j$ to calculate the quadrature term $Q_{ab} = \max(|Q_j|)$, wherein j = 0 to y;

wherein the processor component employs the set of quadrature terms $Q_j$ and the set of in-phase terms $I_k$ to calculate the quadrature term $Q_s$, and the in-phase term $I_s$.

22. The apparatus of claim 21, wherein the processor component calculates a constant $C_1$ and a constant $C_2$, wherein the processor component calculates:

$$Q_s = C_1 \times \sqrt{\sum_{j=0}^{j=y} Q_j^2}\ ;$$

wherein the processor component calculates:

$$I_s = C_2 \times \sqrt{\sum_{k=0}^{k=z} I_k^2}\ ;$$

wherein the processor component calculates the constant $C_1$ and the constant $C_2$ such that a magnitude of the quadrature term $Q_s$, a magnitude of the quadrature term $Q_{ab}$, and a magnitude of the in-phase term $I_s$ comprise a substantially same magnitude at a modulation depth M of an operating range for the phase generated carrier.

23. The apparatus of claim 22, wherein the processor component employs the quadrature term $Q_{ab}$ and the quadrature term $Q_s$ to calculate a correction term $\Delta Q = Q_s - Q_{ab}$;

wherein the processor component employs the quadrature term $Q_s$ and the correction term $\Delta Q$ to calculate a quadrature term $Q_m$;

wherein the processor component employs the quadrature term $Q_m$, the in-phase term $I_s$, the set of quadrature terms $Q_j$, and the set of in-phase terms $I_k$ to calculate the phase angle $\varphi$.

24. The apparatus of claim 23, wherein the processor component employs the quadrature term $Q_m$ and the set of quadrature terms $Q_j$ to calculate a quadrature term Q, wherein the processor component employs the in-phase term $I_s$ and the set of in-phase terms $I_k$ to calculate an in-phase term I;

wherein the processor component calculates:

$Q = \pm Q_m$;

wherein the processor component calculates:

$I = \pm I_s$;

wherein the processor component employs the set of quadrature terms $Q_j$ to determine a sign of Q;

wherein the processor component employs the set of in-phase terms $I_k$ to determine a sign of I;

wherein the processor component calculates:

$\varphi = \text{arctangent}(Q / I)$.

25. The apparatus of claim 24, wherein the processor component calculates a constant $C_3$, wherein the processor component calculates:

$$Q_m = Q_s + (C_3 \times \Delta Q).$$

26. The apparatus of claim 25, wherein x = 7, y = 3, and z = 1;

wherein the processor component calculates:

$Q_0 = S_0 - S_4$, $Q_1 = S_1 - S_5$, $Q_2 = S_2 - S_6$, and $Q_3 = S_3 - S_7$;

wherein the processor component calculates:

$I_0 = (S_0 + S_4) - (S_2 + S_6)$; and

$I_1 = (S_1 + S_5) - (S_3 + S_7)$.

27. The apparatus of claim 25, wherein $x = 15$, $y = 7$, and $z = 3$; wherein the processor component calculates:

$Q_0 = S_0 - S_8$, $Q_1 = S_1 - S_9$, $Q_2 = S_2 - S_{10}$, $Q_3 = S_3 - S_{11}$,

$Q_4 = S_4 - S_{12}$, $Q_5 = S_5 - S_{13}$, $Q_6 = S_6 - S_{14}$, and $Q_7 = S_7 - S_{15}$;

wherein the processor component calculates:

$I_0 = ( S_0 + S_8 ) - ( S_4 + S_{12} )$, $I_1 = ( S_1 + S_9 ) - ( S_5 + S_{13} )$,

$I_2 = ( S_2 + S_{10} ) - ( S_6 + S_{14} )$, and $I_3 = ( S_3 + S_{11} ) - ( S_7 + S_{15} )$.

28. An article, a sensor array that employs a parameter to induce a time-varying phase angle $\varphi$ on an optical signal that comprises a phase generated carrier with a demodulation phase offset $\beta$, the article comprising:

one or more computer-readable signal-bearing media;

means in the one or more media for calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$.

29. The article of claim 28, further comprising:

means in the one or more media for sampling an output signal from the sensor array to obtain a plurality of samples $S_n$, wherein $n = 0$ to x;

wherein the means in the one or more media for calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ comprises:

means in the one or more media for calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of one or more of the plurality of samples $S_n$.

30. The article of claim 29, wherein the means in the one or more media for calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of the one or more of the plurality of samples $S_n$ comprises:

means in the one or more media for calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples $S_n$, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$; and

means in the one or more media for calculating the phase angle $\varphi$ through employment of the one or more quadrature terms and the one or more in-phase terms.

31. The article of claim 29, wherein the output signal comprises a period $T_{pulse}$, wherein the means in the one or more media for sampling the output signal from the sensor array to obtain the plurality of samples $S_n$, wherein n = 0 to x comprises:

means in the one or more media for sampling the output signal from the sensor array to obtain the plurality of samples $S_n$ within a period $T_s$, wherein n = 0 to x , wherein $T_s$ is less than or equal to $1.125 \times T_{pulse}$.

32. The article of claim 31, wherein $T_s$ is less than or equal to $T_{pulse}$.

33. The article of claim 31, wherein the means in the one or more media for calculating the phase angle $\varphi$ independently of the demodulation phase offset $\beta$ through employment of the one or more of the plurality of samples $S_n$ comprises:

means in the one or more media for calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples $S_n$, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset $\beta$;

means in the one or more media for calculating the phase angle $\varphi$ through employment of the one or more quadrature terms and the one or more in-phase terms.

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